# **Road Drainage Alternatives**

By

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"Three of the most important aspects of road design – drainage, drainage, and drainage!"

Keller and Sherar, 2003



## Impacts

Roads can alter both drainage patterns and runoff generation, resulting in:

- Destabilization of side-cast material downslope hillsides;
- Gullying and channel network expansion;
- Increased downstream sediment loads;
- Altered stream flow and channel adjustments;
- Standing water (pothole, sag, rut, wet area) can weaken the subgrade and accelerate erosion and damage to the road.



See Drew Coe's and Mike Wopat's presentations under Series 1





Photo: Matt Boone, RWQCB





Photo: USDA Forest Service





Photo: USDA Forest Service







## **Primary Objective**

Design, construct and maintain roads so they are hydraulically invisible (i.e., water intercepted by roads is returned to natural flow processes as quickly as practical).



## **Remember!**

Successfully treating road drainage (hydraulically invisible)

ally Protecting natural resources

Ensuring full use of road and + <u>reduced</u> <u>maintenance</u> and repair costs



## Outline

Types of road prism shapes

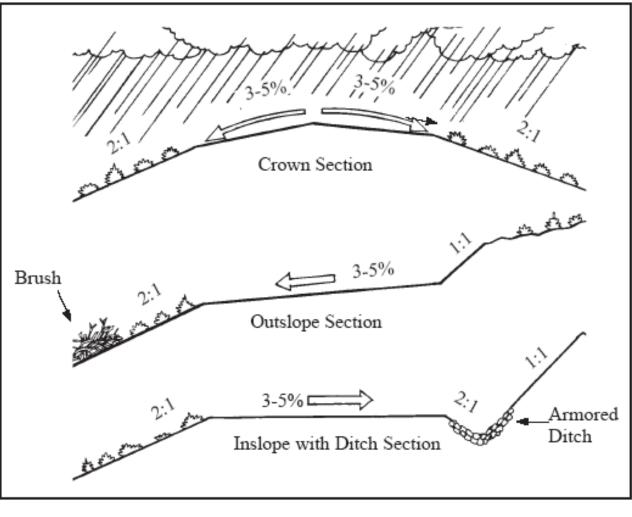
### Drainage structures

- Types
- Spacing
- Location

Ditch and outlet scour protection



## **Road Prism Shapes**







Keller and Sherar, 2003

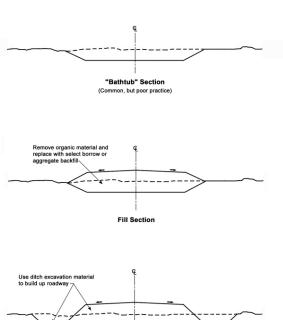


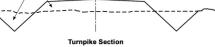
CALFORNA GEOLODICAL SURVEY





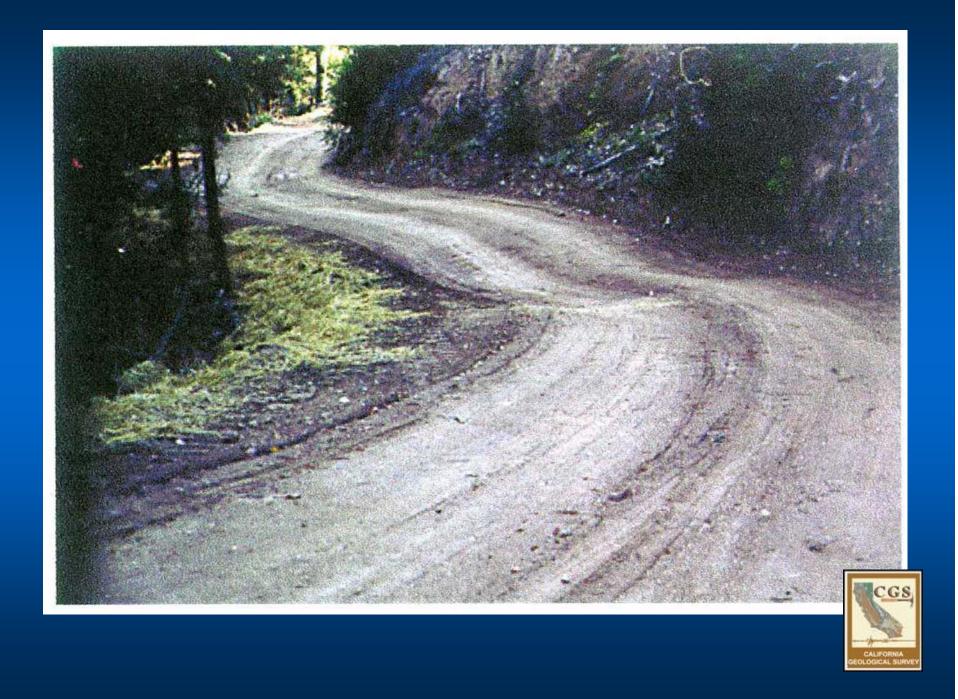






ROAD OPTIONS IN WET, VERY FLAT TERRAIN





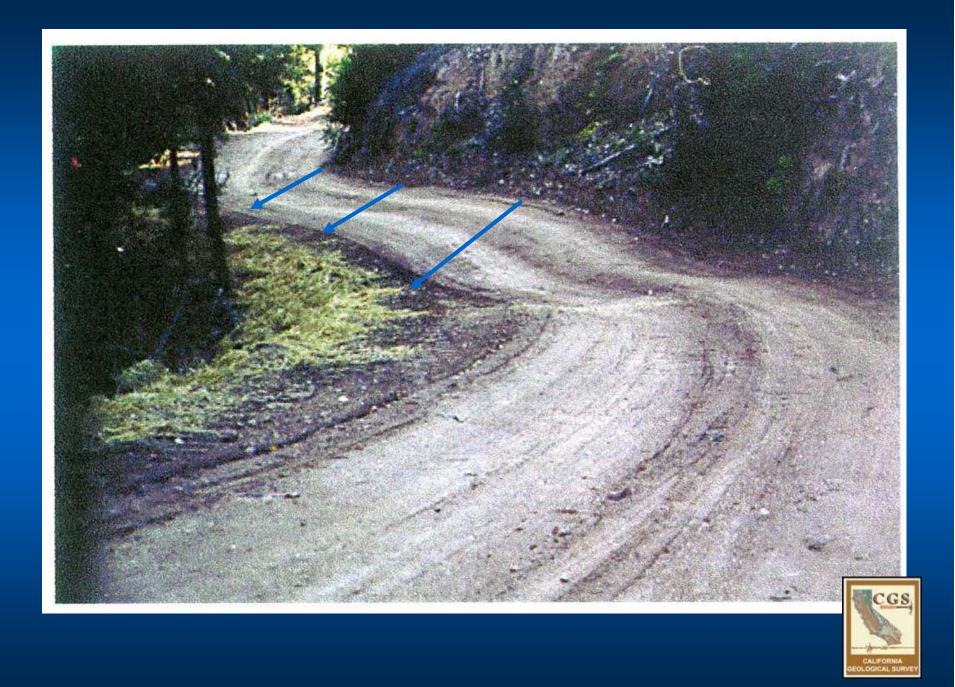






Photo: Matt Boone, RWQCB





Photo: Matt Boone, RWQCB

## **Drainage Structure**

- Inboard Ditches
- Culverts (Crossdrains)
- Rolling Dips
- Waterbars
- Over-side drains/flumes
- Leadouts/ditchouts

- Subdrains
  - Intercept
  - Blanket
- Others
  - Rubber water diverters
  - Open-topped channels
  - Grade Reversals
    and Rolls







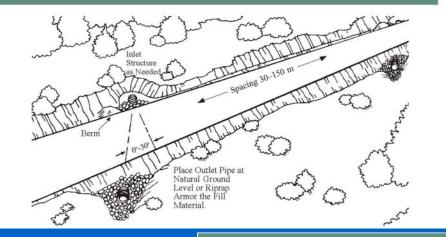
Photo: USDA Forest Service



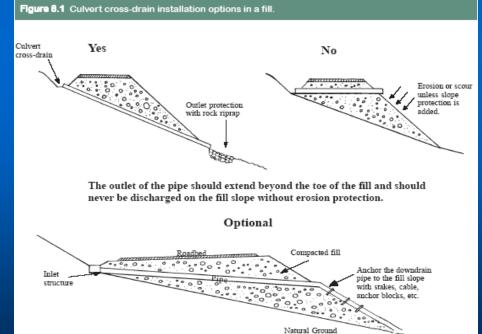




#### Figure 7.4 Culvert cross-drains.



### **Pipe Structures**



Optional use of a downdrain pipe, especially in large fills with poor soils and high rainfall areas, where fill settlement may require culvert repairs.

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Keller and Sherar, 2003

### **Pipe Structures**



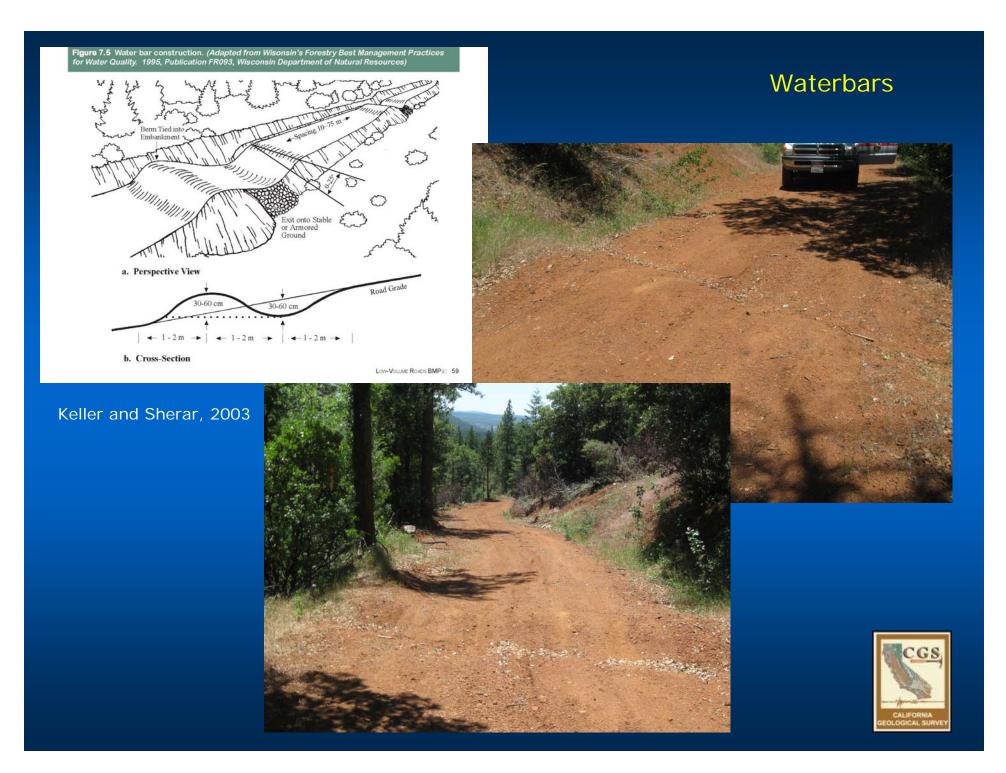




### Pipe Structures

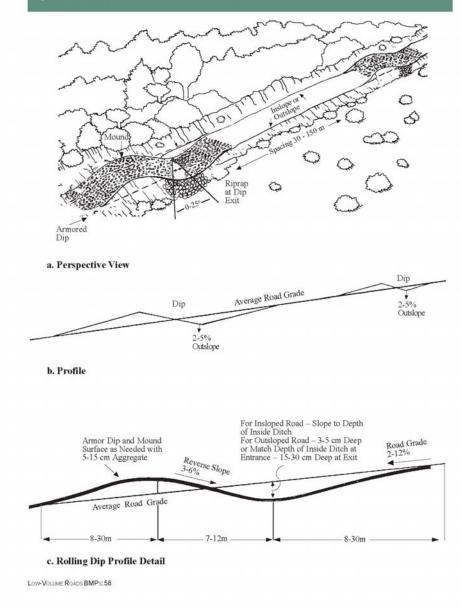






#### Figure 7.3 Rolling (broad-based) dip cross-drains.

### **Rolling Dips**





Keller and Sherar, 2003









Photo: Matt Boone, RWQCB



### Over-side drains



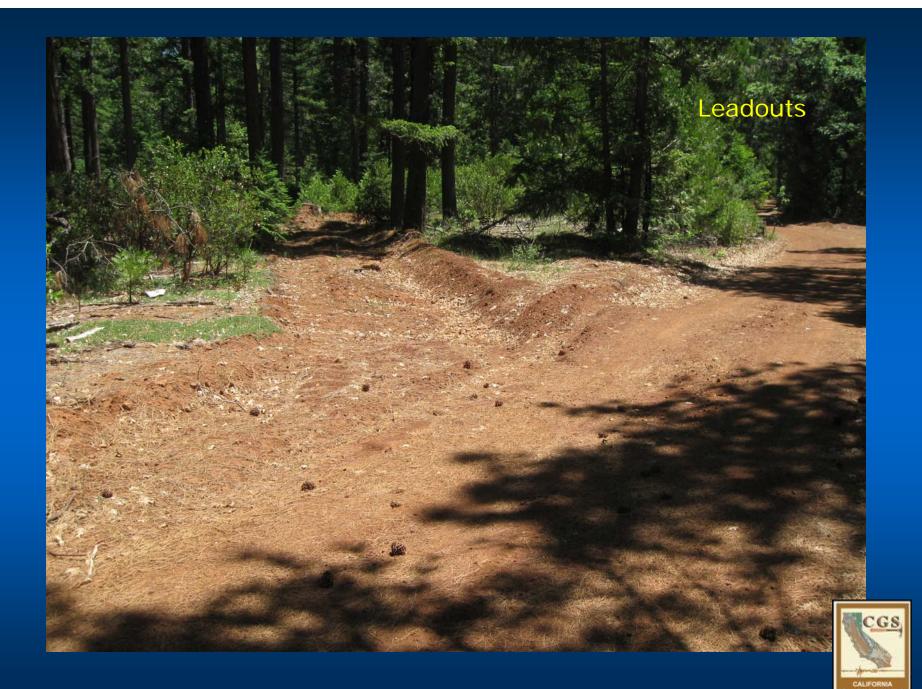
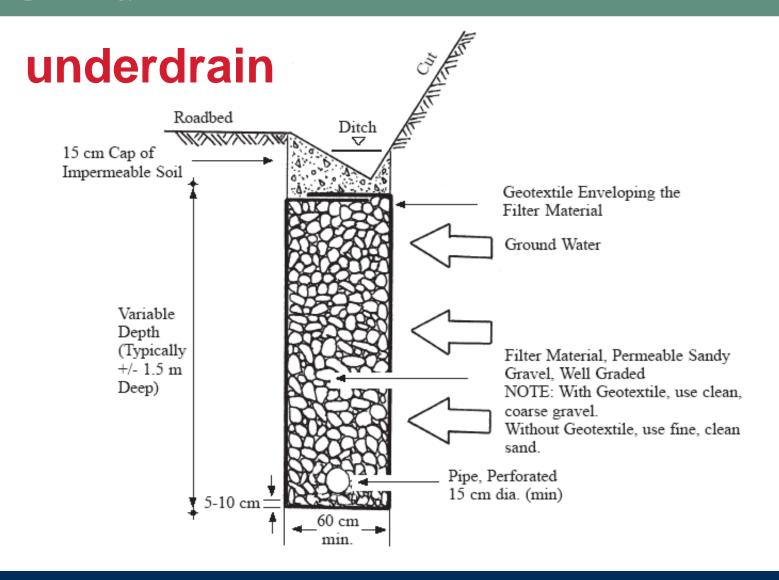


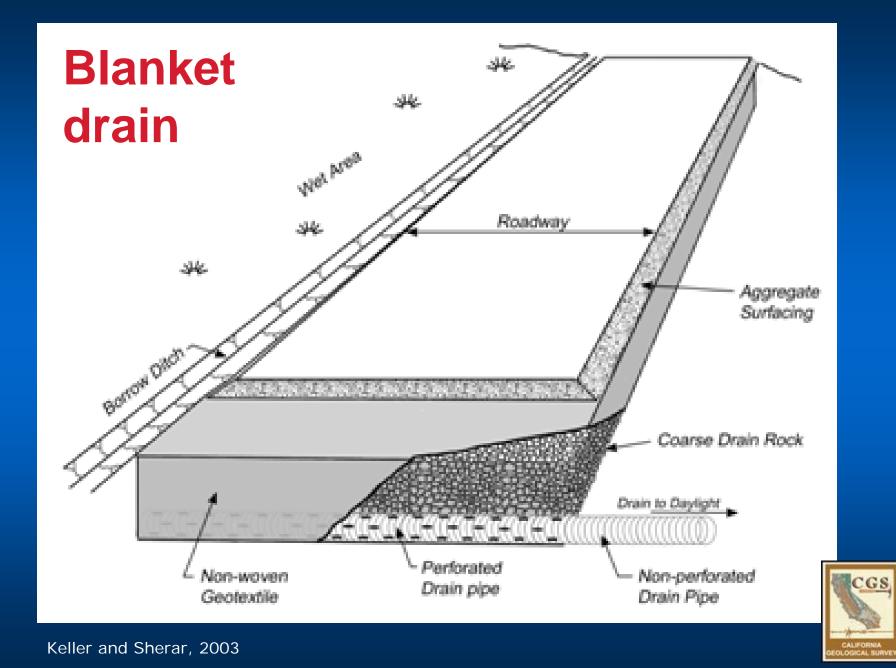


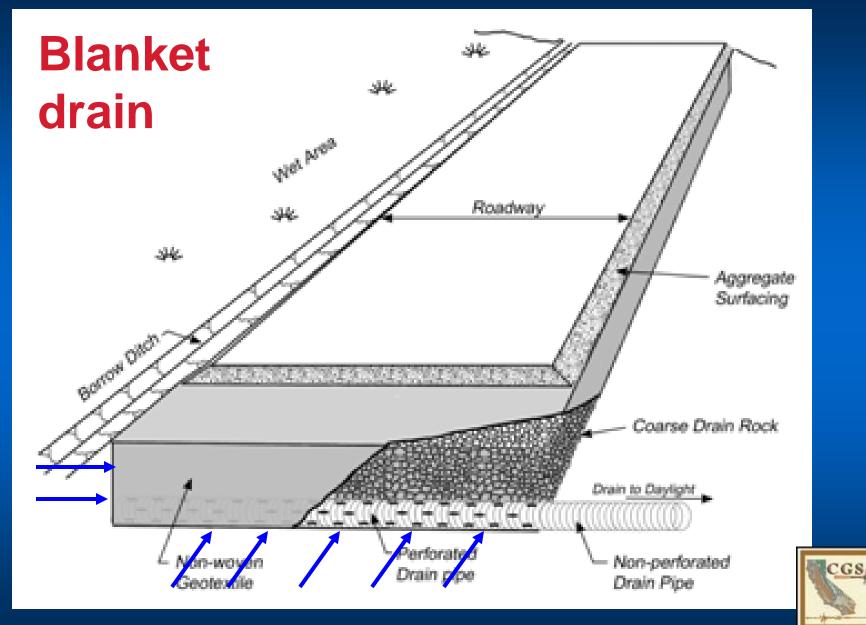


Figure 7.16 Typical road underdrain used to remove subsurface water.



GS





Keller and Sherar, 2003

## Geofabric



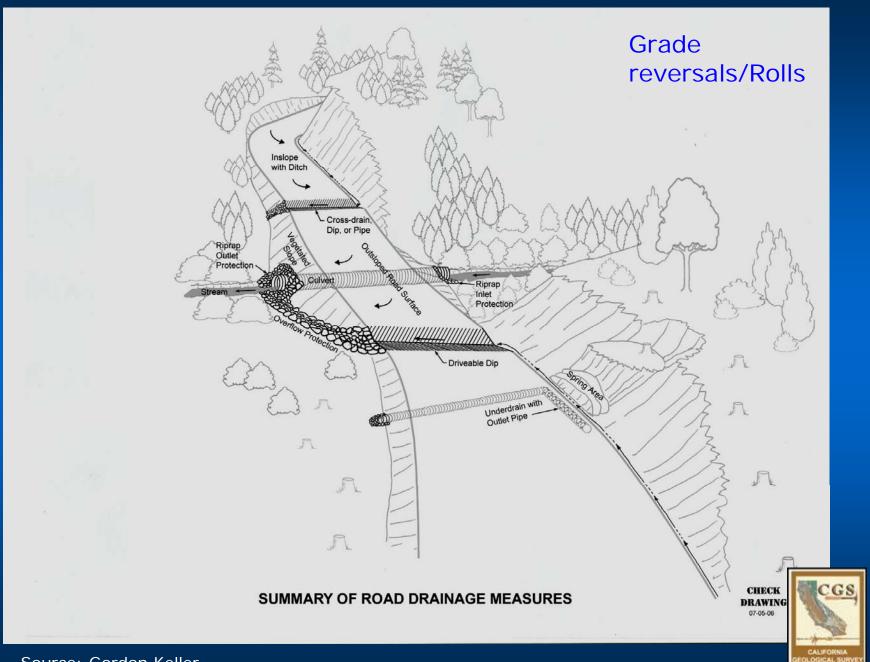
High porosity + High permeability = High flow for longer. High permeability but percent open area (POA) is more prone to clogging.







CALIFORNIA GEOLOGICAL SURVEY



Source: Gordon Keller

# **Questions?**



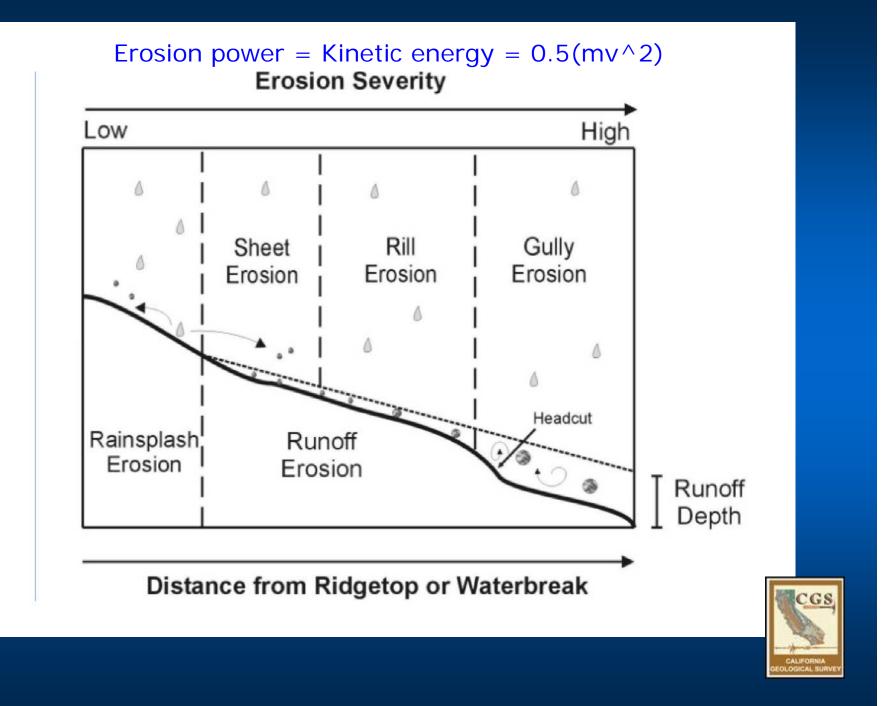
## **Drainage Structure Spacing**

 Drainage structures should be constructed at a spacing that would prevent excessive erosion either in the inboard ditch, along the road surface, or downslope of the road.

## Spacing is a function of:

- Road grade
- Hydrology
- Soil type
- Surfacing
- Modify Structure locations to account for landscape features as necessary (topography, wet areas, landslides, etc).





#### Spacing is a function of:

- •Road grade
- Hydrology
- •Soil type

•Surfacing

Road Grade	Group 1 GW, GP, Aggregate Surfacing	Group 2 GM, GC	Group 3 CH, CL	Group 4 MH, SC, SM	Group 5 & 6 SW, SP, ML	
percent	meters					
2	120	97	75	52	29	
4	103	84	65	45	26	
6	88	71	55	39	23	
8	74	60	47	33	20	
10	61	50	39	28	17	
12	50	41	32	23ª	14ª	
14	42	34°	26°	19*	11°	

Table 4-Guidelines for maximum distance\* between contiguous surface cross drains based on USCS soil erodibility groups<sup>b</sup>.

\*Distance between cross drains should be reduced according to the following (based on Packer and Christensen 1964):

Reduce the distance by: If the road is located:

5 meters	in the middle one-third of a slope
11 meters	in the bottom one-third of a slope
3 meters	on an east or west exposure
6 meters	on a south slope.
*****	

If, after applying the above, the resulting distance is less than 20 meters, set the distance between cross drains at 20 meters and apply aggregate surfacing and erosion protection measures, such as vegetative seeding of road, fills, shoulders, ditches, and embankments.

Copstead, R. L., et al. (1998)

<sup>b</sup>Adapted from the distance recommendations summarized in Table 3, and soil erodibility hierarchy suggested by Gray and Leiser.

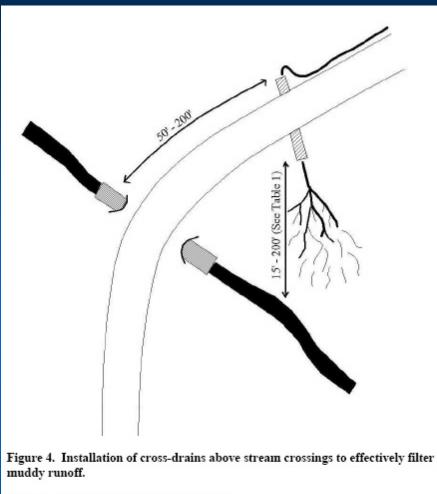
<sup>e</sup>Not recommended for dips because they may require approach grades steeper than 15 percent.



## **Drainage Structure Location**

- 1. Spaced close enough to avoid excessive rilling and gullying.
- 2. Located sufficiently upgrade of watercourse crossings to allow filtering of sediment-rich runoff by the buffer strip between the road and stream.
- 3. Direct discharge away from unstable or potentially unstable areas.
- 4. Upgradient of drainage divides to keep water from one catchment basin mixing with, and potentially impacting, another catchment basin not conditioned to the additional flows.
- 5. Discharge onto divergent (convex) to planar slopes, where possible, to promote better dispersion and infiltration.
- 6. Drain saturated soils of the road prism.
- 7. Upgrade of breaks in the road grade that transition from low-gradient to high-gradient.





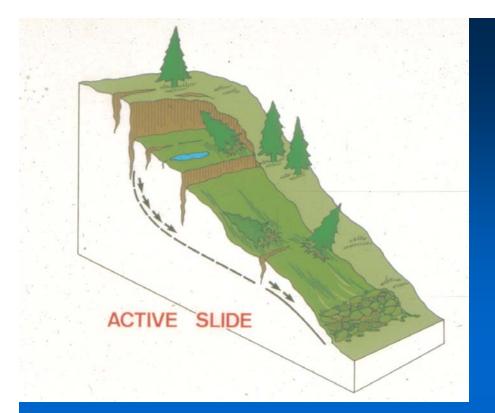
#### Table 1. Suggested distances for filtering

Distance to next cross-drain up road			
under 300 feet	300-600 feet	over 600 feet	
15 ft	30 ft	50 ft	
30 ft	60 ft	100 ft	
50 ft	100 ft	150 ft	
60 ft	120 ft	200 ft	
	under 300 feet 15 ft 30 ft 50 ft	under 300 feet      300-600 feet        15 ft      30 ft        30 ft      60 ft        50 ft      100 ft	

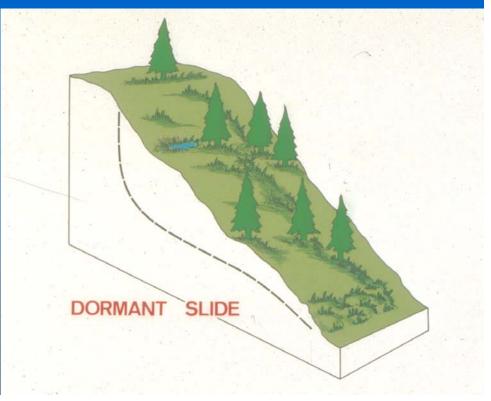
Place upgrade of stream crossings to allow for filtering of sediment-rich runoff prior to entering the stream.



### Oregon Department of Forestry

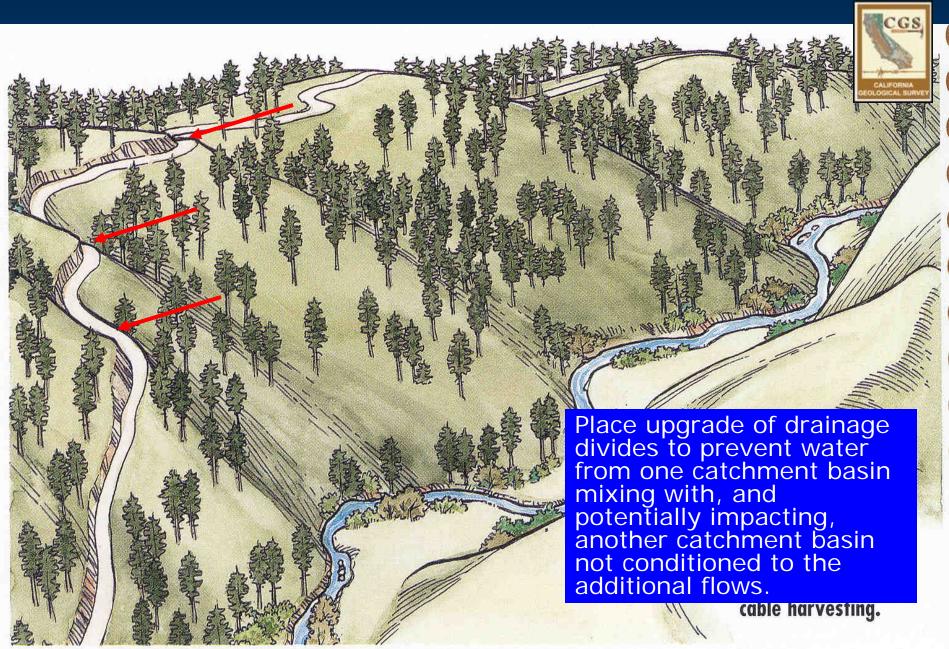


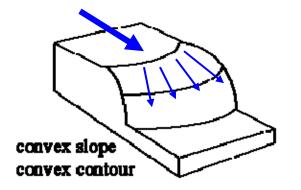
Place to discharge away from unstable or potentially unstable areas.

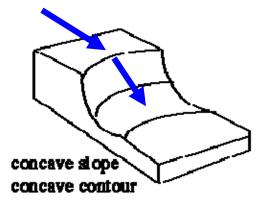






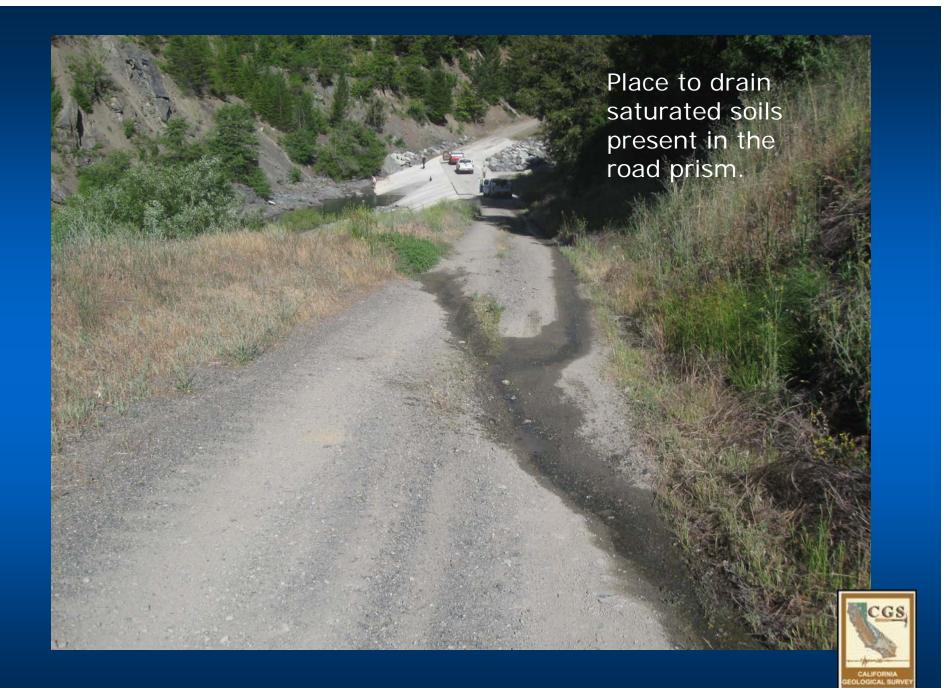


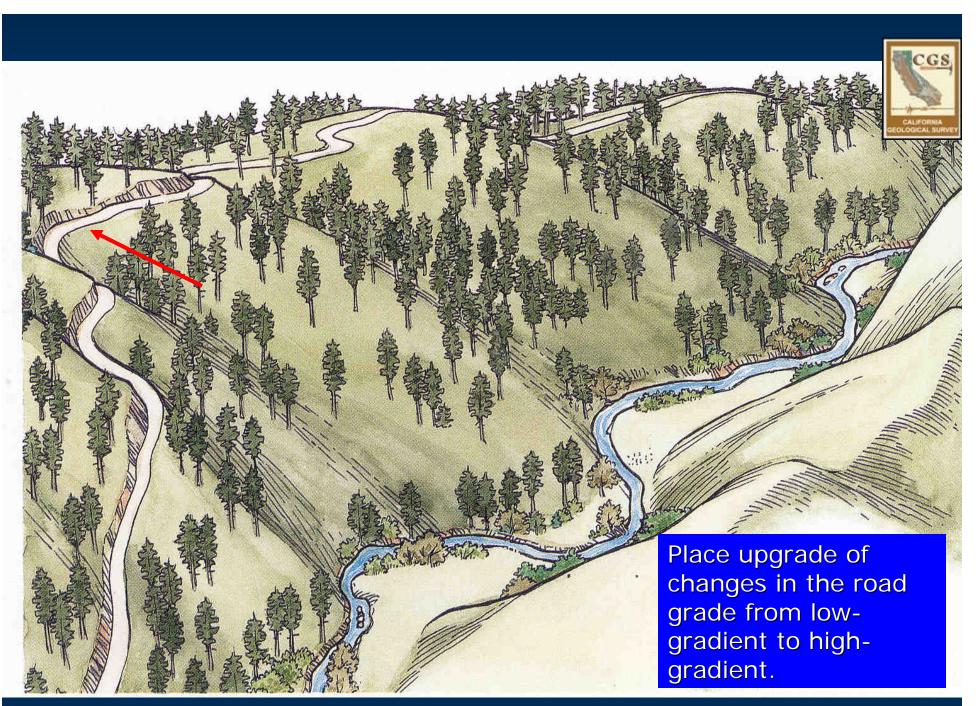




Place to discharge onto divergent (convex) to planar slopes, where possible, to promote better dispersion and infiltration.







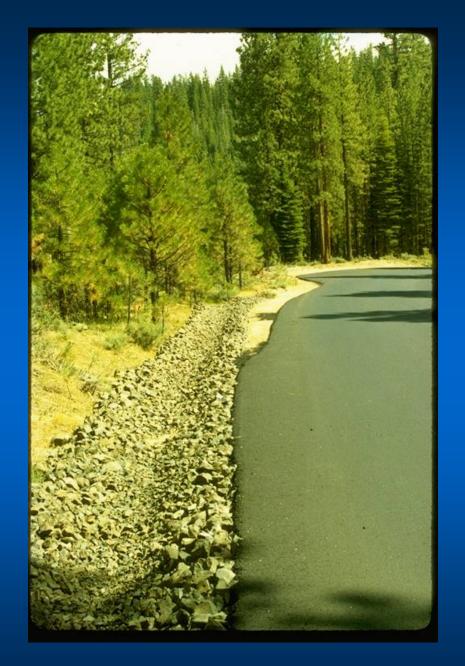
Oregon Forest Resources Institute, 2002

## **Energy Dissipators**

The use and selection of an appropriate energy dissipator should be based on in-field conditions that include:

- Flow
- Soil erodibility
- Slope gradient, and
- Slope roughness and cover





# Ditches













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U.S. Department of Transportation

Federal Highway Administration

Hydraulic Engineering Circular No. 14, Third Edition

### Hydraulic Design of Energy Dissipators for Culverts and Channels



## Storm Water Quality Handbooks

**Project Planning and Design Guide** 

Storm Water Pollution Prevention Plan (SWPPP) and Water Pollution Control Program (WPCP) Preparation Manual

> Construction Site Best Management Practices (BMPs) Manual



State of California Department of Transportation

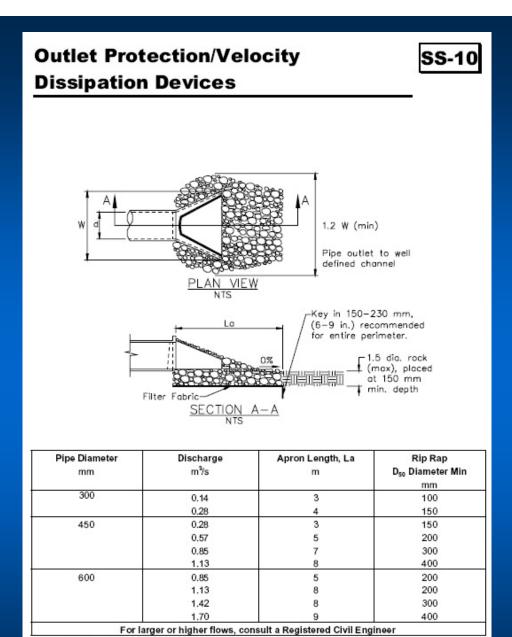
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March 2003











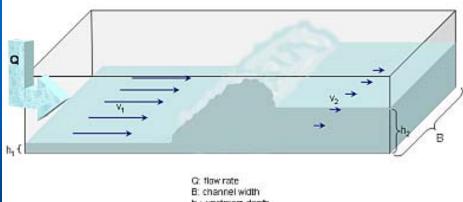
Source: USDA - SCS

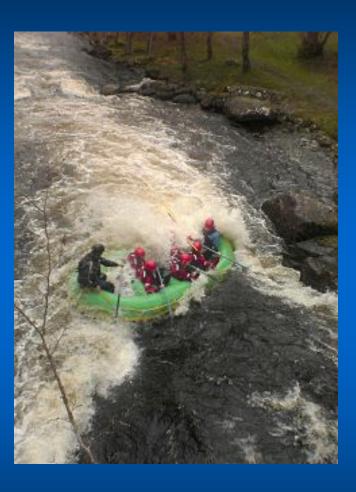


Caltrans Storm Water Quality Handbooks Construction Site Best Management Practices Manual March 1, 2003 Section 3 Outlet Protection/Velocity Dissipation Devices \$\$.10 3 of 3

### Stilling basin / tailwater







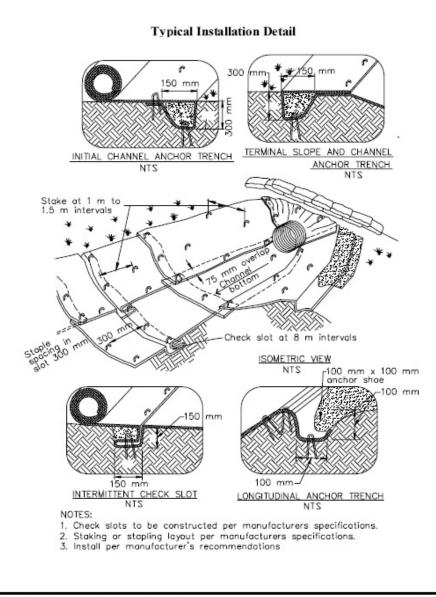
G: flow rate B: channel width h<sub>1</sub>: upstream depth v<sub>1</sub>: upstream velocity h<sub>2</sub>: downstream depth v<sub>2</sub>: downstream velocity



Figure: Brian McNoldy

#### Geotextiles, Mats, Plastic Covers and Erosion Control Blankets







Caltrans Storm Water Quality Handbooks Construction Site Best Management Practices Manual March 1, 2003 Section 3 Geotextiles, Mats, Plastic Covers and EC Blankets SS-7 10 of 11



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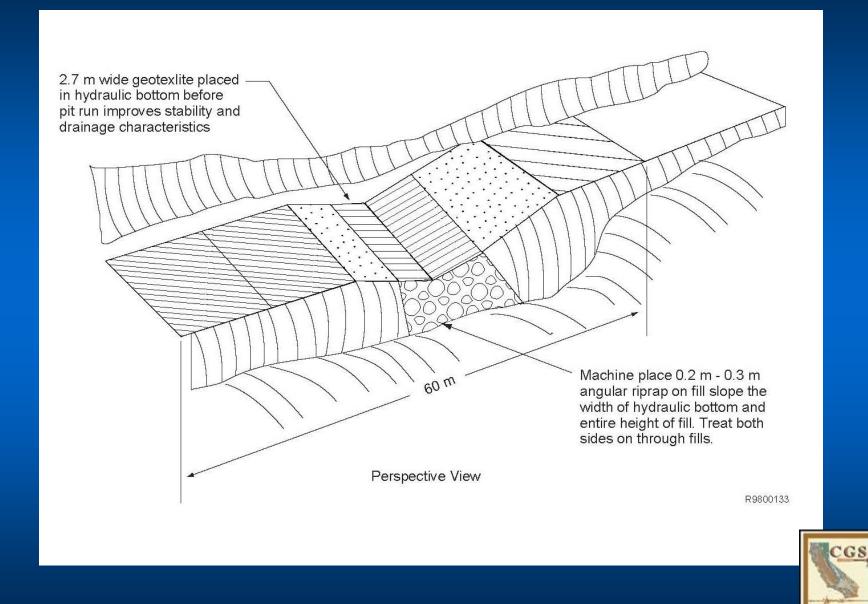


Photo: Matt Boone, RWQCB





Photo: Matt Boone, RWQCB



Copstead, R. L., et al. (1998)

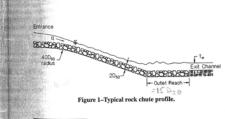
#### DESIGN OF ROCK CHUTES

#### K. M. Robinson, C. E. Rice, K. C. Kadavy

ABSTRACT. Rock chute design information is consolidated from several sources to provide a comprehensive design tool. The rock slope stability, boundary roughness, and outlet stability of rock chutes are each discussed. Tests were performed in three rectangular flumes and in two full size structures. Angular riprap with a median stone size ranging from 15 to 278 mm was examined on rock chutes with slopes ranging from 2 to 40%. The typical mode of channel failure is described. An empirical prediction equation is presented relating the highest stable discharge on a rock chute to the median stone size and the bed slope. A boundary roughness relationship is also presented that relates the Manning roughness coefficient to the median stone size and bed slope. These tests also suggest that the riprap size required for stability on the slope will remain stable in the outlet reach even with minimal tailwater. This article contains information needed to perform a rock chute design.

Keywords. Rock chutes, Riprap, Channel design, Hydraulics, Stability, Roughness, Grade control.

ock chutes or loose-riprap-lined channels are recent investigations. The objective of this article is to used to safely convey water to a lower elevation. present pertinent information from several sources to These structures provide an alternative method of protecting the soil surface to maintain a stable slope and to dissipate a portion of the flow energy. Watershed management applications for this type of structure are numerous such as channel stabilization, grade control, and embankment overtopping. Depending on the availability and quality of accessible rock materials, rock chutes may offer economic advantages over more traditional structures. Flow cascading down a rock chute is visually pleasing, and these structures offer aesthetic advantages for sensitive locations. Construction of these chutes can be performed with unskilled labor and a comparatively small amount of equipment. A typical rock chute profile is shown in figure 1.



Article was submitted for publication in September 1997; reviewed and approved for publication by the Soil & Water Div. of ASAE in March 1998. Presented as ASAE Paper No. 97-2062.

The authors are Kerry M. Robinson, P.E., ASAE Member Engineer, Research Hydraulic Engineer, Charles E. Rice, P.E. ASAE Member Engineer, Research Hydraulic Engineer, and Kem C. Kadavy, P.E., ASAE Member Engineer, Agricultural Engineer, USDA ARS, Stillwater, OK. Corresponding author: Kerry M. Robinson, 1301 N. Western St., Stillwater, OK 74075; tel: (405) 624-4135; fax: (405) 624-4136; e-mail: krob@ag.gov.

Vol. 41(3):621-626

Transactions of the ASAE

1998 American Society of Agricultural Engineers

621

Robinson, K.M., Rice, C.E., and Kadavy, K.C., 1998, Design of Rock Chutes, Transactions of the ASAE, Vol. 41(3): 621-626

RELATED WORK

Rock chutes in various forms have been used for many years. Isbash (1936) examined the ability of flowing water to move rocks. The shape of a rock fill cross-section was described while stone of a known size and weight was deposited in flowing water. Isbash developed a relationship describing the minimum velocity necessary to move stones of a known size and specific gravity. Anderson et al. (1970) developed a design procedure for riprap-lined drainage channels by testing rounded stone on relatively flat slopes. Uniformly sized riprap materials remained stable at higher flow rates than non-uniform materials. The non-uniform materials enhanced the protection of the filter material below the rock layer. Wittler and Abt (1990) found that the stone gradation has a significant influence on chute performance. The uniformly sized riprap withstood higher flow rates than non-uniform material of the same D<sub>50</sub>. The uniform material did fail more suddenly than the nonuniform materials once the slope became unstable.

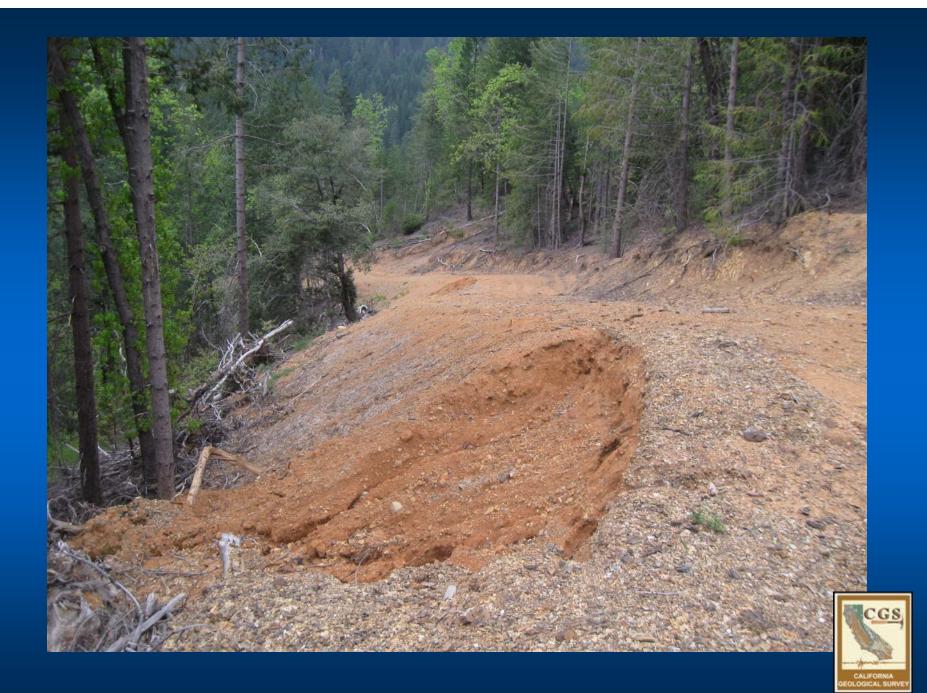
Rock chute structures have been the subject of several

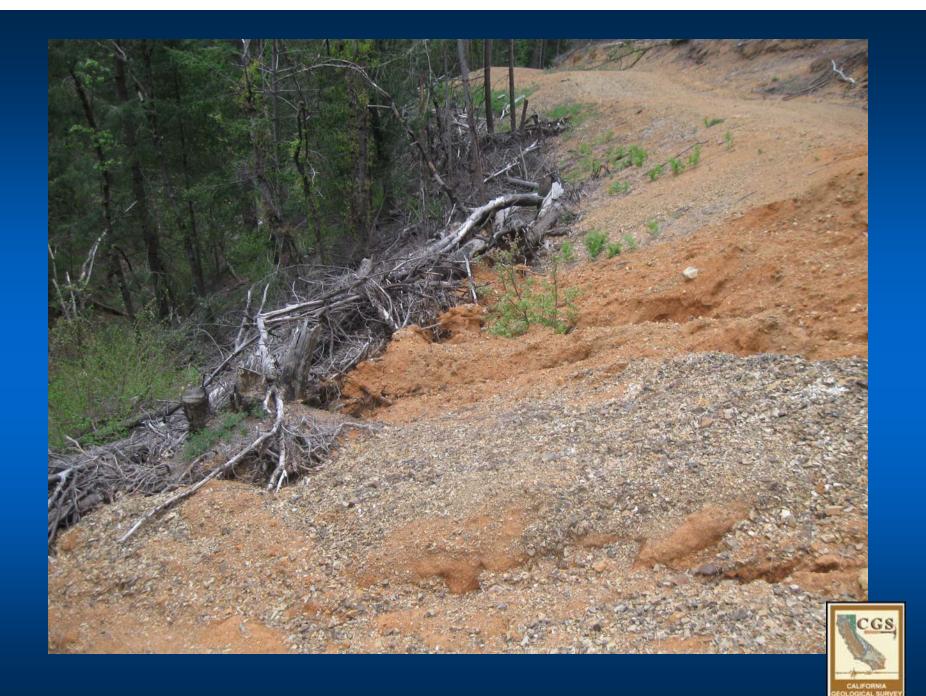
provide the designer with a comprehensive design tool.

Abt et al. (1987) and Abt and Johnson (1991) tested both angular and rounded stone and found that the rounded stone failed at a unit discharge of approximately 40% less than angular shaped stones of the same median stone size. These researchers developed design criteria for median stone sizes between 25 and 152 mm on slopes ranging between 1 and 20%.

Maynord (1988) developed a riprap sizing method for stable open channel flows on slopes of 2% or less. This design method, based on the average local velocity and flow depth, used the D30 as the characteristic rock size. The effects of riprap gradation, thickness, and shape were also examined. Maynord (1992) extended this design method to slopes between 2/and 20% for nonimpinging flows. Frizell

FaRXZO





## **Remember!**

Successfully treating road = natural drainage

Protecting resources

**Ensuring full** use of road and + reduced maintenance and repair costs



# **Questions?**

